

Figure 2 : laser beam profile in far field (a) and polarisation ellipsoid (b).

Using a 8W pump power source, 15 kHz of PRF has been reached, allowing hundreds of lidar signals to be averaged on each line of sight and thus speckle noise to be reduced.

### Optical architecture

The optical architecture (Figure 3) is based on collimated beams, and so can be used with different fiber lasers, even with multimode fibers, since the laser output is collimated in free space. A compact circulator, based on Brewster and quarter wave plates has been specially designed, with both robustness and very good optical isolation (60 dB). A refractive afocal telescope gives to the output beam an effective Gaussian diameter of 50mm (at  $1/e^2$ , with  $M2=1.4$ ), allowing a focus range up to 300m.

The received beam is reflected by the Brewster plate and focused on a single mode PM fiber before being mixed with the fibered Local Oscillator.

The oscillator beam is frequency shifted by 70MHz before being amplified by the EDFA, allowing the sign of the Doppler shift to be measured.

The Figure 3 illustrates the lidar setup.

EDFA : Fiber Doped Power Amplifier CL : collimating lens,  
BP : Brewster plate, FM: folding mirror, QWP: Quarter  
Wave Plate, L1-L2 : afocal telescope, FL: Focusing lens

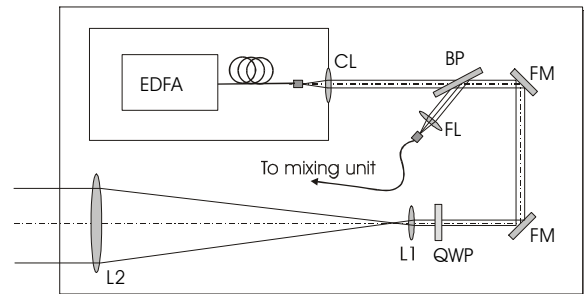


Figure 3 : Lidar setup

### LIDAR PERFORMANCES

Taking into account the geometric and energetic lidar parameters, as well as atmospheric parameters, CNR and velocity resolution profiles can be derived from propagation models.

The figure above compares the theoretical CNR profile and the actual profile. The backscattering coefficient is assumed to be  $\beta_{\pi}=3.5 \cdot 10^{-7} \text{ m}^{-1} \text{ sr}^{-1}$ .

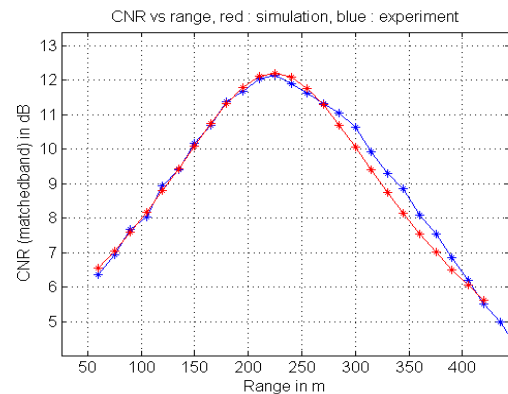


Figure 4: Theoretical and experimental CNR profile

These end-to-end models, developed at Onera were formerly used for the lidar and laser design.

## SIGNAL PROCESSING

### Signal acquisition

The signal is sampled and processed in real time by a DSP board. The signal is analysed by 64 points FFT, giving a basic range resolution of 37.5 meters, and a velocity resolution of 3 m/s . 60 samples overlap between successive FFTs gives a measurement spectrum every 2.4 m. With a 15 kHz PRF, 100 spectra averaging and 15°/s scan speed , an angular resolution as good as 0.1 ° is obtained ( 35 cm at 200m). The averaged spectra are then stored for high level processing.

### Man Machine Interface

In order to display the wake vortices measurements in real time, three maps are computed, having range and angle as main axes. These maps are calculated with the three first moments of the spectra, delivering respectively the CNR, the velocity centroid, and the velocity dispersion maps.

The CNR map is useful for the lidar alignment setting and focus adjustment. The velocity map gives the position and trajectory of the vortex cores. The dispersion map informs on wind turbulence.

Figure 5 shows a capture of the real time display showing a wake vortex pair 325 m away from the Lidar . Y axis is the range in m from the Lidar , X axis is the index of line of sight, linearly dependant of the scan angle. The scanner executes symmetric saw tooth trajectories so that right part of the display appears symmetric from left hand side. The color scale gives the velocity information (spectrum centroid value) on each point of the scan plane. The real time display does not inform about the maximum velocity component in the spectra, related to the wake vortex circulation. However, the presence and position of a wake vortex is clearly visible on the velocity map: wake vortex has a characteristic signature which allows the operator to stop the record when the vortex has disappeared.

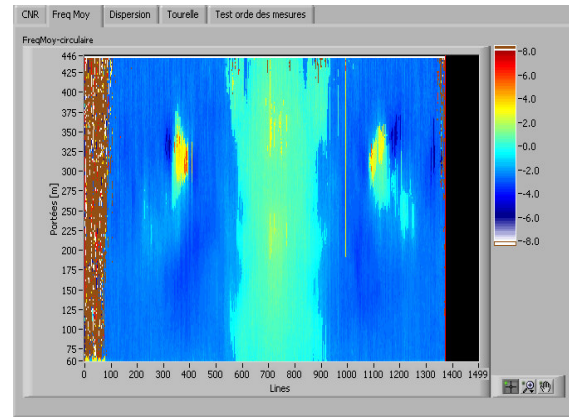


Figure 5 : Real time display of velocity map.

### Post processing and wake vortex monitoring

Two signal processing methods for wake vortex analysis have been previously developed for 2  $\mu\text{m}$  pulsed lidars. One is based on parametric estimation<sup>4,5</sup>, and the other one is a direct method<sup>6</sup>. The outputs are vortex positions and vortex circulation as a function of time.

We have chosen to explore both methods. Comparative results with those algorithms will be presented. Figure 6 shows maximum and minimum velocity envelopes of DLR method for a scan for a wake vortex measurement in low altitude and high signal to noise ratio conditions. Each line represents a different range. X axis is the time. Y axis represents scan angle and velocity in arbitrary units. In this case, maxima measured velocity are  $\pm 15$  m/s. Positions of both wake vortices are obtained considering the coordinates (range and angle) of max velocity and min velocity for each vortex .

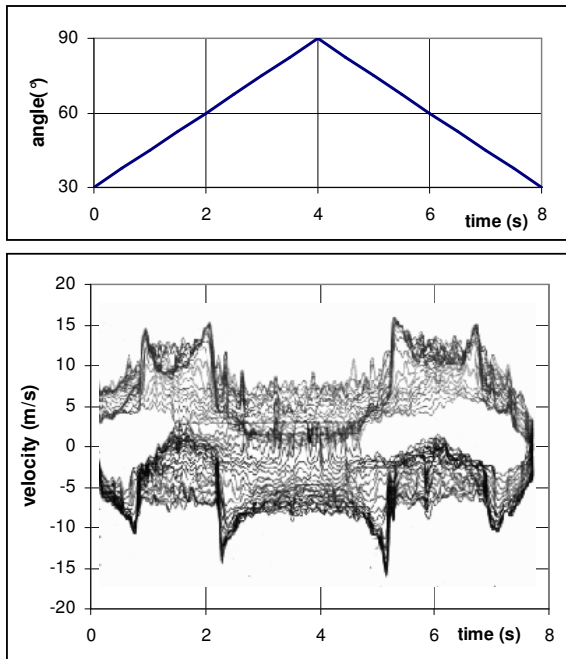


Figure 6 : Scan pattern and velocity profiles at different ranges.

## CONCLUSIONS

This paper illustrates the good results obtained with a pulsed lidar based on MOPFA 1.5 $\mu$ m laser, for detection and monitoring of wake vortices on airport fields. Operational ranges larger than 400m have been demonstrated, with a 60 $\mu$ J, 15kHz, 250ns pulse fiber doped Er laser. Wake profiles, positions and circulations can be derived from recorded data. During the next months, the system will be automated and miniaturized by Leosphere for a future deployment on airports.

Increasing the power of fiber lasers remains a topic of interest at Onera/Dota, and longer range wind lidars (800m) are expected soon.

## REFERENCES

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